

14 APR 2004



PRIORITY DOCUMENT

SUBMITTED OR TRANSMITTED IN
COMPLIANCE WITH RULE 17.1(a) OR (b)

The Patent Office
Concept House
Cardiff Road
Newport
South Wales
NP10 8QQ

REC'D 14 APR 2004

WIPO PCT

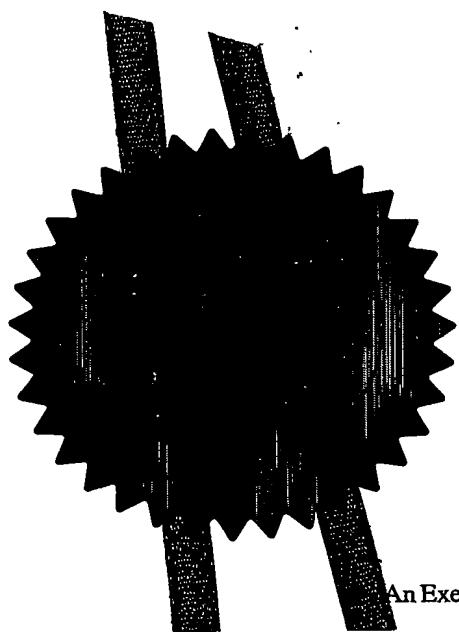
I, the undersigned, being an officer duly authorised in accordance with Section 74(1) and (4) of the Deregulation & Contracting Out Act 1994, to sign and issue certificates on behalf of the Comptroller-General, hereby certify that annexed hereto is a true copy of the documents as originally filed in connection with the patent application identified therein.

I also certify that the application is now proceeding in the name as identified herein.

In accordance with the Patents (Companies Re-registration) Rules 1982, if a company named in this certificate and any accompanying documents has re-registered under the Companies Act 1980 with the same name as that with which it was registered immediately before re-registration save for the substitution as, or inclusion as, the last part of the name of the words "public limited company" or their equivalents in Welsh, references to the name of the company in this certificate and any accompanying documents shall be treated as references to the name with which it is so re-registered.

In accordance with the rules, the words "public limited company" may be replaced by p.l.c., plc, P.L.C. or PLC.

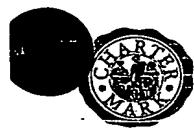
Re-registration under the Companies Act does not constitute a new legal entity but merely subjects the company to certain additional company law rules.



Signed

Dated 6 April 2004

BEST AVAILABLE COPY



GB0306646.1

By virtue of a direction under Section 32 of the patents Act 1977, the application is proceeding
in the name of,

CALTEC LIMITED,
Incorporated in the United Kingdom,
The Innovation Centre,
Cranfield,
BEDFORD,
MK43 0BT,
United Kingdom

[ADP No. 08646879001]

Patents Form 1/77

9. Enter the number of sheets for any of the following items you are filing with this form.
Do not count copies of the same document

Continuation sheets of this form

Description	
10	
Claim(s)	4
Abstract	
Drawing(s)	4

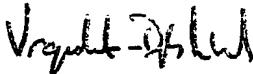
10. If you are also filing any of the following, state how many against each item.

Priority documents	-
Translations of priority documents	-
Statement of inventorship and right to grant of a patent (Patents Form 7/77)	-
Request for preliminary examination and search (Patents Form 9/77)	1
Request for substantive examination (Patents Form 10/77)	-
Any other documents (please specify)	-

11.

I/We request the grant of a patent on the basis of this application.

Signature



Date 20.03.03

12. Name and daytime telephone number of person to contact in the United Kingdom

Mr Simon Raynor - 01908 666645

Warning

After an application for a patent has been filed, the Comptroller of the Patent Office will consider whether publication or communication of the invention should be prohibited or restricted under Section 22 of the Patents Act 1977. You will be informed if it is necessary to prohibit or restrict your invention in this way. Furthermore, if you live in the United Kingdom, Section 23 of the Patents Act 1977 stops you from applying for a patent abroad without first getting written permission from the Patent Office unless an application has been filed at least 6 weeks beforehand in the United Kingdom for a patent for the same invention and either no direction prohibiting publication or communication has been given, or any such direction has been revoked.

Notes

- a) If you need help to fill in this form or you have any questions, please contact the Patent Office on 08459 500505.
- b) Write your answers in capital letters using black ink or you may type them.
- c) If there is not enough space for all the relevant details on any part of this form, please continue on a separate sheet of paper and write "see continuation sheet" in the relevant part(s). Any continuation sheet should be attached to this form.
- d) If you have answered 'Yes' Patents Form 7/77 will need to be filed.
- e) Once you have filled in the form you must remember to sign and date it.
- f) For details of the fee and ways to pay please contact the Patent Office.

A SYSTEM AND METHOD FOR PUMPING MULTIPHASE FLUIDS

The present invention relates to a system and method for pumping multiphase fluids, and in particular but not exclusively to a system and method for sustainable oil 5 production boosting.

Production from many oil and gas fields is restricted as the reservoir pressure drops during the field life. Generally, the producing wells have to operate at a pressure which is demanded by the downstream process or pipeline system and the flowing wellhead pressure can not be dropped below this limit in order either to maintain production or to 10 increase production and recovery from the field. Under these conditions a pressure boosting system is required so that the reduction in the back pressure on wells or the flowing wellhead pressure is achieved while meeting the downstream process or pipeline pressure requirements.

The productivity of wells within a production system or field varies because of a 15 number of reasons such as fragmentation of the reservoir, where production comes from different zones or from satellite fields. In these cases it is very common that some wells are classed as good high pressure producers while some could be poor low pressure wells.

In many conventional production systems the flow from all producing wells is combined 20 in a manifold and the total products enter one or a series of separators. These separators separate primarily gas and liquid phases. The pressure of the separated gas is in most cases boosted using compressors to achieve a high pressure which is needed either for export of the gas by pipeline or to allow the gas to be used for other purposes, such as for use as lift gas or for injection into the reservoir to maintain the 25 reservoir pressure.

The compressors are designed with a minimum required inlet pressure and it is this pressure which dictates the operating pressure of the separators upstream of the compressors. As the pressure of the reservoir drops, the required minimum inlet pressure for the compressors becomes a limiting factor as the flowing wellhead 30 pressure of the producing wells cannot be allowed to drop further to maintain or increase production. This situation may also apply to fragmented reservoirs or fields with satellites which in part may have a different productivity level or permeability

compared to the rest of the field. In this case it is these parts or wells from these low pressure fragmented parts that need boosting. However, lowering the inlet pressure of compressors reduces their gas handling capacity.

Furthermore, upgrading of such compressors so that a lower inlet pressure can be
5 handled (providing a lower back pressure on the wells and more production) is a very
costly operation and also requires a long lead time. Although this upgrading is done in
some fields which are in the later stage of their production life, this upgrading is not
considered for many marginal fields because of its high cost.

In these circumstances a boosting system which would allow some or all the low
10 pressure wells to operate at a lower back pressure (and therefore a higher production
rate) would be highly desired. Such a boosting system would enable production from
the selected low pressure wells to be increased without the need to spend large sums
upgrading the entire production system. Even in cases when the final upgrading of the
15 process and compression system takes place, such projects often take two years or
more to complete and interrupt production during this period. A boosting system that
could be implemented at relatively low cost would be well justified as an interim
solution, because the boosting system would pay for the capital spent within a few
months while the remaining time would bring added revenue to the operator.

There are a variety of ways by which the boost in pressure or the reduction in the back
20 pressure on producing wells can be achieved. The selection of a suitable system is
affected by field conditions and constraints and the economic aspects which relate to
key parameters such as the capital cost, operation cost, increase in production and
revenue and factors such as payback period for the investment made.

An ideal system is one that is of relatively low cost, simple to operate and reliable,
25 while delivering the boost required.

Boosting the production of oil involves handling both gas and liquid phases as in
practically all cases the produced oil is in multiphase form (containing gas and liquid
phases). In order to increase the pressure of the produced fluids the either boosting
30 system has to be capable of handling the multiphase mixture, requiring equipment
such as multiphase pumps, or alternatively the gas and liquid phases can be separated
and a separate boosting system used for each phase. This means, for example, using
a gas compressor for boosting the gas phase and a liquid booster pump for the liquid
phase. The so called multiphase booster pumps that can handle both gas and liquid

phases are complex and costly units and the operation conditions they face and have to cope with are the main cause of their complexity and high cost. Some typical operating requirements for such pumps are:

- Handling two phase flow
- 5 • Coping with chaotic fluctuating flow regimes associated with multiphase flow such as slug flow.
- The ability to run for a short period of time with 100% gas and no liquid phase. This condition again is often generated as a result of flow regime or slugging in pipelines in inclined, horizontal or vertical configuration.
- 10 • The ability to handle a large volume of gas compared to the associated liquid phase. This is particularly true for low pressure wells (as the volume of gas increases as the pressure decreases) and wells that are gas lifted (where gas is injected within the well bore to reduce the hydrostatic head of the fluids in the well bore and maximise the flowing wellhead pressure). In most cases the gas/liquid ratio of the mixture at the operating conditions ranges from 9 to 49 or higher. This means that the volume of the gas as the percentage of the total mixture is between 15 90% and 98% or higher.

The relatively large volume of gas compared to the liquid phase alone raises the power requirement for the multiphase pump by several fold and in some cases ten fold or

20 more. This large power requirement is a major setback for many fields, and particularly on satellite platforms, which do not have sufficient power available for this purpose. A typical range of the power required for multiphase pumps is 200kW to 1000kW and in some cases even higher, reaching 2 to 3 megawatt, most of which is caused by the large volume of gas involved.

25 An alternative system which uses a jet pump and was the subject of European Patent No. 0717818, uses high pressure (HP) wells as the source of energy to reduce the back pressure on low pressure (LP) wells and thus increase their production rate while meeting the downstream system pressure requirement. This system works satisfactorily in many applications but has limitations when either:

- 30 • the gas volume fraction of the LP wells is very high;

- the available high pressure wells are not likely to maintain their high pressure for long, or
- the pressure and flow rate of high pressure wells are not significantly higher than those of the selected LP wells.

5 Another boosting system, which is marketed under the trade name Wellcom Boost, includes an option as shown in Figure 1 where a multiphase gas and oil mixture from one or more LP wells is supplied through a manifold 2 to a separator 4, which in this case is a compact cyclonic type separator. The gas and liquid phases are separated and a booster pump 6 is used to boost the pressure of the LP liquid phase. This
10 boosted liquid phase is fed to the HP inlet of a jet pump 8 and is used as the motive flow. The separated LP gas is fed through a bypass line 10 to the LP inlet of the jet pump 8. The LP gas pressure is boosted by the jet pump 8 to deliver a gas/liquid mixture into a pipeline 12 at the required discharge pressure.

A drawback of this system is that it does not operate satisfactorily in conditions when
15 the volumetric flow rate of the LP gas is high in comparison with the volumetric flow rate of the boosted liquid phase. Typically, when the volumetric flow rate of the LP gas at the operating pressure and temperature is more than twice that of the liquid phase the effectiveness of the jet pump system drops significantly, making the system unattractive and uneconomical. In practically all oil fields the ratio of gas to liquid flow
20 rate is well above 2 at the operating conditions (often between 5 to 50) so the system shown in figure 1 has a very limited application.

If other conventional boosting options are used, such as using a liquid booster pump (for the liquid phase) and a compressor (for the separated gas phase), the system becomes highly complex and costly as a result of the need to have a separation
25 system to separate gas and liquid phases as well as the compressor and the booster pump. In this case the compressor is the major cost item, which brings about further drawbacks including requiring considerable space, high maintenance requirements and a long lead delivery period.

According to the present invention there is provided a system for pumping multiphase
30 fluids, the system including a phase separator that is connected to receive a LP multiphase fluid, and is constructed and arranged to separate a LP gas phase and a LP liquid phase from the LP multiphase fluid; a gas-gas jet pump having a LP inlet connected to receive the LP gas phase from the phase separator, a HP inlet connected

to receive HP gas supplied from a sustainable gas source, and an outlet for providing outlet gas at a pressure higher than that of the LP gas phase; and a liquid pump having a LP inlet connected to receive the LP liquid phase from the phase separator, and an outlet for providing outlet liquid at a pressure higher than that of the LP liquid phase.

- 5 The sustainable gas source may be from a supply of lift gas or export gas. The sustainable gas source may include a compressor. Advantageously, the sustainable gas source has a pressure at least twice, and preferably several times, that of the LP gas phase. Typically the pressure may be in the range 100-150 bar.

The gas-gas jet pump may typically have an outlet pressure in the range 1.1 to 3.2

- 10 times that of the LP gas, although it is not limited to this range.

The liquid pump may be a mechanical pump, and is preferably a positive displacement pump. The outlet pressure of the liquid pump is preferably similar to that of the gas-gas jet pump.

Alternatively, the liquid pump may be a liquid-liquid jet pump having a LP inlet

- 15 connected to receive the LP liquid phase from the phase separator, a HP inlet connected to receive a HP liquid supply from a sustainable liquid source, and an outlet for providing outlet liquid at a pressure higher than that of the LP liquid phase. The sustainable liquid source may be injection water or a supply of export oil, or any other suitable HP liquid supply. The sustainable liquid source may have a pressure at least
20 twice that of the LP liquid phase. The liquid-liquid jet pump preferably has an outlet pressure similar to that of the gas-gas jet pump.

The system may include a knock-out vessel for removing retained liquid from the LP gas phase. The knock-out vessel preferably has a liquid outlet connected to deliver the removed liquid to the liquid pump.

- 25 The separator may be a cyclone type separator.

The system may include a commingling device connected to the outlets of the jet pump and the liquid pump, for combining the outlet gas and the outlet liquid and providing a combined multiphase outlet fluid at a pressure higher than that of the LP multiphase fluid. The mixing device may be a commingler.

- 30 The combined multiphase outlet fluid may have an outlet pressure in the range 1.1 to 3.2 times that of the LP liquid phase, although it is not necessarily limited to this range. The multiphase fluid is preferably a petroleum gas/oil mixture. The gas/liquid ratio of

the petroleum gas/oil mixture may be in the range of 9 to 49, as dictated by field conditions.

According to another aspect of the invention there is provided a method of pumping multiphase fluids, the method including separating a LP multiphase fluid into a LP gas phase and a LP liquid phase, increasing the pressure of the LP gas phase using a gas-
5 phase and a LP liquid phase, increasing the pressure of the LP gas phase using a gas-
gas jet pump by supplying a HP gas supply from a sustainable gas source to a HP inlet
of the jet pump and supplying the LP gas phase to a LP inlet of the jet pump, and
increasing the pressure of the LP liquid phase using a liquid pump.

10 The method may also include mixing the increased pressure gas and liquid phases to provide a combined multiphase fluid at a pressure higher than that of the LP multiphase fluid

Further novel aspects of the invention include the following:

15 • A system consisting of a gas-liquid separator, a gas-gas jet pump, a booster pump and commingler in the arrangement shown in Figure 2.

• A system which uses a sustainable source of high pressure gas as the motive flow to the jet pump (e.g. lift gas).

• A system with a pump which is capable of not only handling the liquid phase but can also handle some free gas. The need for gas handling capability arises for two main reasons:-

20 a) the separated liquid phase is live unstabilised crude oil and is subject to the release of gas from the fluid as it passes along the pipework;

b) often as a result of inherent flow fluctuations (or flow regime) upstream and/or as a result of using compact separators such as cyclonic separators there is some carryover of the gas into the liquid phase.

25 An example of such a pump is the so called Positive Displacement (PD) pump such as twin screw type or progressive cavity type or any other type with such a capability.

• A bypass pipeline system (with its associated control valve) for the pumping system which is used for two main functions:-

- a) to bypass the liquid flow into the pump at the start of the system operation (start-up) to ensure that the pump does not run with 100% gas at start-up;
 - b) to make it possible to recirculate some of the liquid in cases when the liquid flow rate handled by the pump is well below its optimum design value.
- 5 • A set of check valves to prevent reverse flow from one line into the other. These are needed to protect the pump and the other components during any malfunctions.
- The use of sustainable HP liquid phase such as injection water or HP export oil as the motive flow for the liquid phase (option 2).
- 10 • A system that reduces significantly the amount of gas to be handled by the multiphase pump. The reduction in the amount of gas handled by the multiphase pump has the major advantage of reducing the size of the pump, reducing the power required for the pump significantly and reducing the cost because of the said reduction in size and power for the pump. It also has the advantage of enabling the boosting system to be used on locations where high electric power (100 to 2000kW typically) is not available for use by the multiphase pumps alone.
- 15

Embodiments of the invention will now be described, by way of example, with reference to the accompanying drawings, in which:

20 Figure 1 illustrates diagrammatically the general configuration of a prior art pressure boosting system, known as the WELLCOM BOOST system;

Figure 2 shows the general configuration of a pressure boosting system according to a first embodiment of the invention;

Figure 3 illustrates an optional modification of the system shown in Figure 2, and

Figure 4 illustrates a second optional modification of the system shown in Figure 2.

25 The general layout and key components of the system are shown in Figure 2. The system includes a separator 14, which is arranged to receive a multiphase fluid mixture (including gas and liquid phases) from one or more LP wells through a manifold 16. Preferably, the separator 14 is a compact cyclone separator, for example as described in European Patent Nos. 1028811 and 1028812. However, other types of separator
30 may alternatively be used including, for example, a conventional gravity separator.

The separator 14 separates the gas and liquid phases, which leave the separator through a gas line 18 and a liquid line 20.

Preferably, a knock-out vessel 22 is provided downstream of the separator 14 to separate any small amounts of liquid that may be carried over by the separated gas phase. The clean LP gas leaves the knock-out vessel 22 through a gas line 24. Some carry over of liquid in the separated gas phase is often expected either because of flow fluctuations, which are common to multiphase flow in pipelines upstream of the system, or as a result of using a compact separator of any kind, as these are more sensitive to flow fluctuations. Alternatively, the knock-out vessel may be omitted, in which case the first gas line 18 is connected directly to the second gas line 24.

The clean LP gas passes via a pressure control valve 26 and a non-return valve 28 to the LP inlet of a gas-gas jet pump 30. The jet pump 30 receives the separated LP gas as the suction flow. High pressure gas is supplied to the HP inlet of the jet pump 30 through a HP gas line 32. The HP gas is preferably obtained from an existing sustainable high pressure source, such as a supply of lift gas or from the downstream side of an existing compressor. The HP gas serves as the motive gas for the jet pump 30 and draws the LP gas through the gas line 24 to provide a combined gas flow at the outlet of the jet pump 30, which is at a substantially higher pressure than the LP gas.

The liquid phase leaves the separator 14 through the liquid line 20 and flows via a control valve 34 to a booster pump 36, which receives the separated liquid phase and boosts its pressure to that required by the downstream system. Any liquid separated from the LP gas in the knock-out vessel 22 flows through a liquid line 38 and a level control valve 40, and is recombined with the main liquid phase in a commingler 42, upstream of the booster pump 36. The pressure boosted liquid phase leaves the booster pump through a liquid line 44, via a non-return valve 46. A bypass line 48 that includes a bypass valve 50 extends from the inlet to the outlet of the booster pump 36.

The pressure boosted liquid phase is delivered through the liquid line 44 and a further non-return valve 52 to a first inlet of a commingler 54, where it is recombined with the increased pressure gas, which is fed to a second inlet of the commingler 54 from the outlet of the jet pump 30, via a gas line 56 and a non-return valve 58. The role of the commingler 54 is to combine the boosted gas and liquid phases efficiently for transportation of the mixture along a single outlet line 60. Alternatively a T-junction may be used to combine the two streams, although this option is less efficient and could cause a minor additional loss of pressure.

This system by the nature of its arrangement and design has the following main advantages.

- It uses HP gas from an existing source that can provide a sustainable very high pressure gas as dictated by its application, such as gas lift.

5 • The pressure of the HP gas remains high and does not drop during the field life, unlike situations when HP gas from existing high pressure wells is used (which is subject to decline in pressure during field life).

10 • The boosting of the liquid phase is achieved by a booster pump that is designed and supplied for each specific application, and therefore its pressure boosting capability will not decline during the field life.

15 • The combination of a jet pump using very high pressure gas from a sustainable source and a booster pump that handles only the liquid phase enables a much higher level of boost in pressure (dp) and/or a reduction on the back pressure of LP wells to be achieved. This, in turn, results in a much higher level of production from LP wells in comparison with other boosting systems that use fluid from HP wells as the motive flow.

20 • The increase in production and recovery is achieved over a much longer period, as the sources of HP fluids (gas or liquid) are sustainable, unlike the HP wells.

A modified form of the pressure boosting system described above is shown in Figure 3.

25 This modified system is suitable for use in situations where a high pressure liquid phase is available from other sources, such as water from a water injection system or export oil that has been boosted to a high pressure for export by pipeline. In this case the booster pump shown in Figure 2 is not used and a much simpler and cheaper option, using a liquid-liquid jet pump 62, is adopted. The high pressure liquid phase is fed to the liquid-liquid jet pump 62 through a liquid line 64 and is used as the motive flow to boost the pressure of LP liquid phase. The other parts of the system are substantially as described above.

30 A second modified form of the pressure boosting system described above is shown in Figure 4. This modified system, is suitable for use in situations where the gas and liquid phases are to be stored or delivered separately. In this case the commingling device 54 is omitted and the HP gas and liquid phases are delivered separately

through supply lines 56', 44' respectively. The other parts of the system are substantially as described above.

CLAIMS

1. A system for pumping multiphase fluids, the system including:
 - a phase separator that is connected to receive a LP multiphase fluid, and is constructed and arranged to separate a LP gas phase and a LP liquid phase from the LP multiphase fluid;
 - a gas-gas jet pump having a LP inlet connected to receive the LP gas phase from the phase separator, a HP inlet connected to receive a HP gas supply from a sustainable gas source, and an outlet for providing outlet gas at a pressure higher than that of the LP gas phase;
 - and a liquid pump having a LP inlet connected to receive the LP liquid phase from the phase separator, and a outlet for providing outlet liquid at a pressure higher than that of the LP liquid phase.
2. A system according to claim 1, wherein the sustainable gas source comprises a supply of lift gas.
3. A system according to claim 1, wherein the sustainable gas source comprises a supply of export gas.
4. A system according to any one of the preceding claims, wherein the sustainable gas source includes a compressor.
5. A system according to any one of the preceding claims, wherein the HP gas supply has a pressure at least twice that of the LP gas phase.
6. A system according to any one of the preceding claims, wherein the gas-gas jet pump has an outlet pressure in the range 1.1 to 3.2 times the pressure of the LP multiphase fluid.
7. A system according to any one of the preceding claims, wherein the liquid pump is a mechanical pump.
8. A system according to claim 7, wherein the liquid pump is a positive displacement pump.

9. A system according to claim 7 or claim 8, wherein the liquid pump has an outlet pressure similar to that of the gas-gas jet pump.
10. A system according to any one of claims 1 to 6, wherein the liquid pump is a liquid-liquid jet pump having a LP inlet connected to receive the LP liquid phase from the phase separator, a HP inlet connected to receive a HP liquid supply from a sustainable liquid source, and an outlet for providing outlet liquid at a pressure higher than that of the LP liquid phase
11. A system according to claim 10, wherein the sustainable liquid source comprises a supply of injection water.
12. A system according to claim 10, wherein the sustainable liquid source comprises a supply of export oil.
13. A system according to any one of the preceding claims, wherein the sustainable liquid source has a pressure at least twice that of the LP liquid phase.
14. A system according to any one of the preceding claims, wherein the liquid-liquid jet pump has an outlet pressure in the range 1.1 to 3.2 times that of the LP liquid phase.
15. A system according to any one of the preceding claims, including a knock-out vessel for removing retained liquid from the LP gas phase.
16. A system according to claim 15, wherein the knock-out vessel has a liquid outlet connected to deliver removed liquid to the liquid pump.
17. A system according to any one of the preceding claims, wherein the separator is a cyclone type separator.

18. A system according to any one of the preceding claims, including a mixing device connected to the outlets of the jet pump and the liquid pump, for combining the outlet gas and the outlet liquid and providing a combined multiphase outlet fluid at a pressure higher than that of the LP multiphase fluid
19. A system according to claim 18, wherein the mixing device is a commingler.
20. A system according to claim 18 or claim 19, wherein the combined multiphase outlet fluid has an outlet pressure in the range 1.1 to 3.2 times that of the LP liquid phase.

21. A system according to any one of claims 18 to 20, wherein the multiphase fluid is a petroleum gas/oil mixture.
22. A system according to claim 21, wherein the gas/liquid ratio of the petroleum gas/oil mixture is in the range 9 to 49.
23. A method of pumping multiphase fluids, the method including:
 - separating a LP multiphase fluid into a LP gas phase and a LP liquid phase;
 - increasing the pressure of the LP gas phase using a gas-gas jet pump, by supplying a HP gas supply from a sustainable gas source to a HP inlet of the jet pump and supplying the LP gas phase to a LP inlet of the jet pump;
 - and increasing the pressure of the LP liquid phase using a liquid pump.
24. A method according to claim 23, wherein the sustainable gas source comprises a supply of lift gas.
25. A method according to claim 23, wherein the sustainable gas source comprises a supply of export gas.
26. A method according to any one of claims 23-25, wherein the sustainable gas source has a pressure at least twice that of the LP gas phase.
27. A method according to any one of claims 23-26, wherein the gas-gas jet pump has an outlet pressure in the range 1.1 to 3.2 times the pressure of the LP multiphase fluid.
28. A method according to any one of claims 23-27, wherein the liquid pump is a mechanical pump.
29. A method according to claim 28, wherein the liquid pump has an outlet pressure in the range 1.1 to 3.2 times the pressure of the LP multiphase fluid.
30. A method according to any one of claims 23 to 27, wherein the liquid pump is a liquid-liquid jet pump having a LP inlet connected to receive the LP liquid phase, and a HP inlet connected to receive a HP liquid supply from a sustainable liquid source.

31. A method according to claim 30, wherein the sustainable liquid source comprises a supply of injection water.
32. A method according to claim 31, wherein the sustainable liquid source comprises a supply of export oil.
33. A method according to any one of claims 23-32, wherein the sustainable liquid source has a pressure at least twice that of the LP multiphase fluid.
34. A method according to any one of claims 23-33, wherein the liquid-liquid jet pump has an outlet pressure in the range 1.1 to 3.2 times that of the LP multiphase fluid.
35. A method according to any one of claims 23-34, in which retained liquid is removed from the LP gas phase using a knock-out vessel.
36. A method according to claim 35, wherein removed liquid is delivered to the liquid pump.
37. A method according to any one of claims 23-36, wherein the LP gas and liquid phases are separated in a cyclone type separator.
38. A method according to any one of claims 23-37, including mixing the increased pressure gas and liquid phases to provide a combined multiphase fluid at a pressure higher than that of the LP multiphase fluid
39. A method according to claim 38, wherein increased pressure gas and liquid phases are mixed in a commingler.
40. A method according to any one of claims 38-39, wherein the combined multiphase outlet fluid has an outlet pressure in the range 1.1 to 3.2 times that of the LP multiphase fluid.

41. A method according to any one of claims 38-40, wherein the multiphase fluid is a petroleum gas/oil mixture.
42. A method according to claim 41, wherein the gas/liquid ratio of the petroleum gas/oil mixture is in the range 9 to 49.

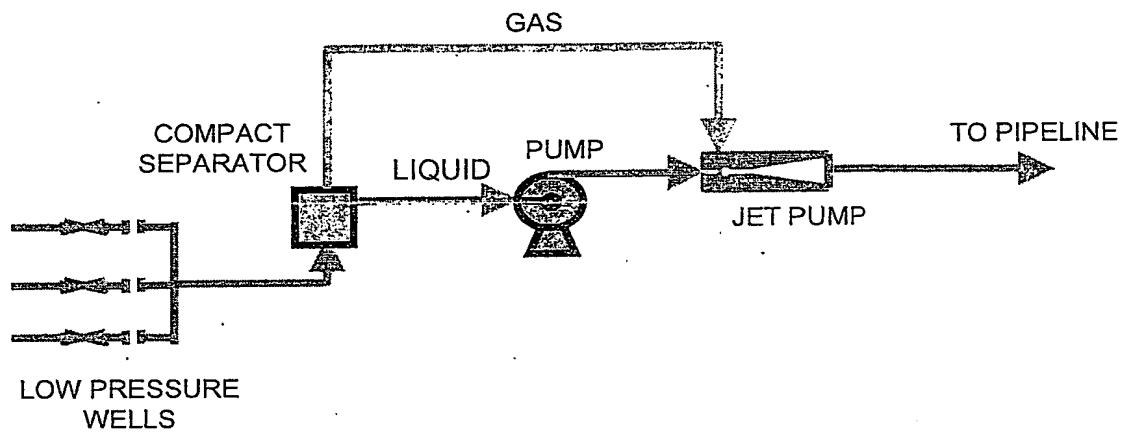


Figure 1 General Configuration of WELLCOM BOOST system

214

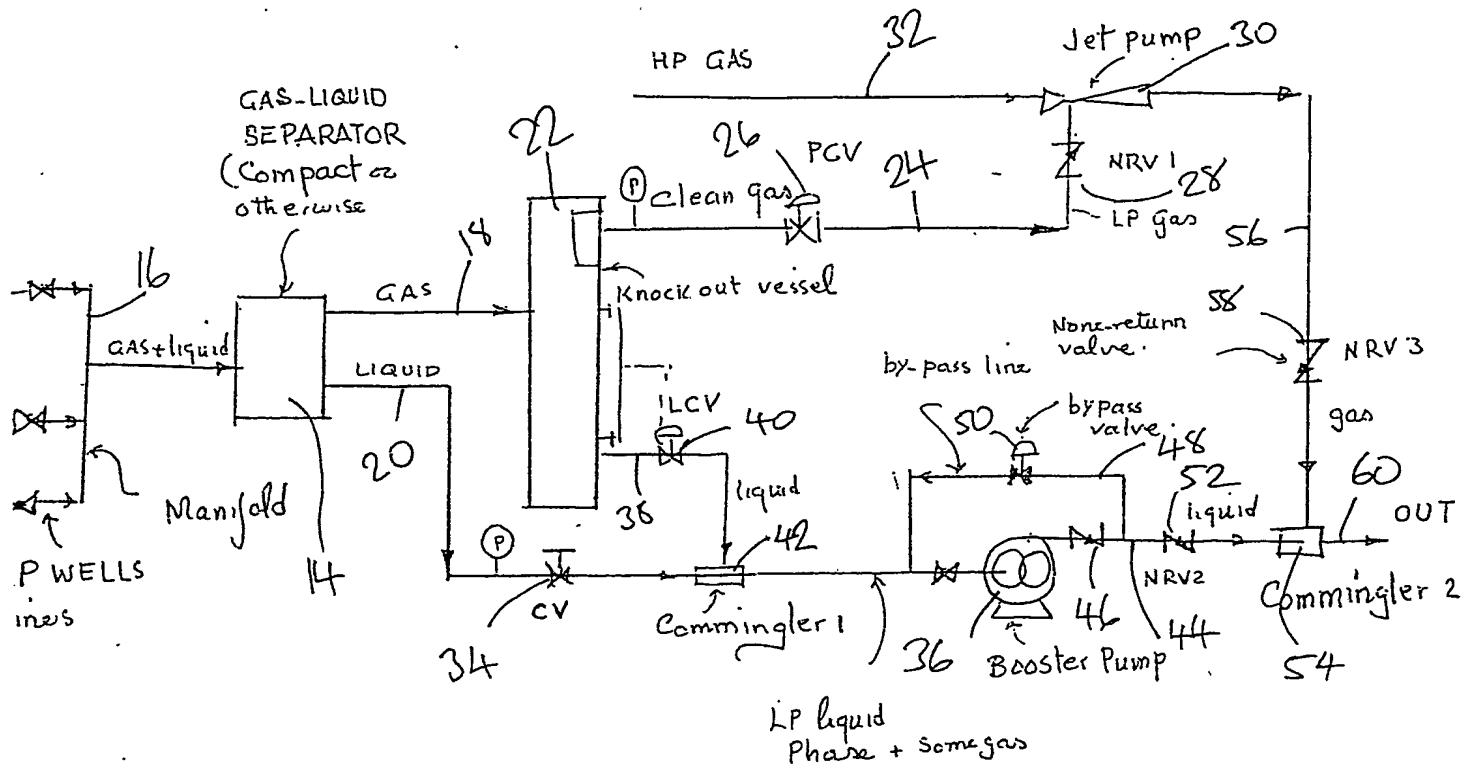


FIGURE 2.

$$3 \longdiv{4}$$

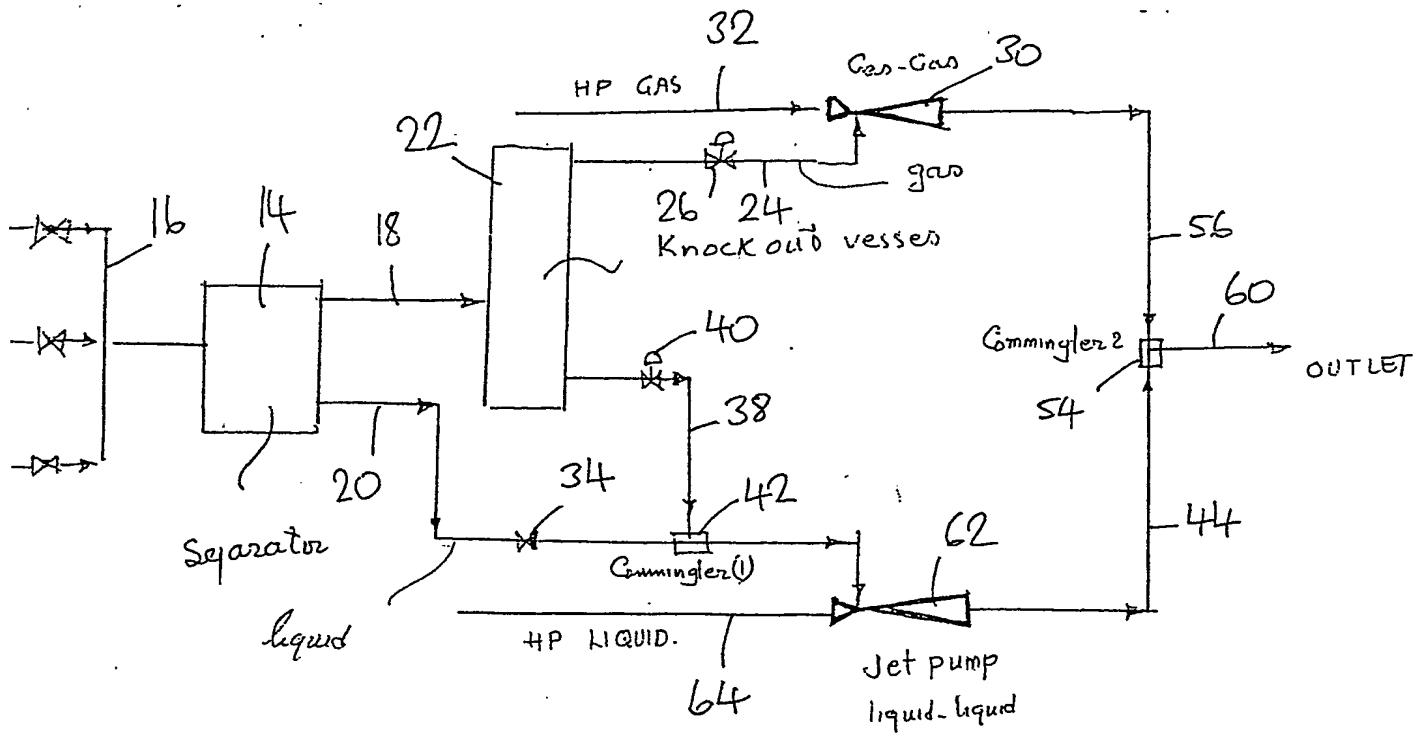


FIGURE 3. ~~OPTION 2~~ USE OF HP liquid & GAS
TO BOOST PRODUCTION USING TWO JET PUMPS

4/4

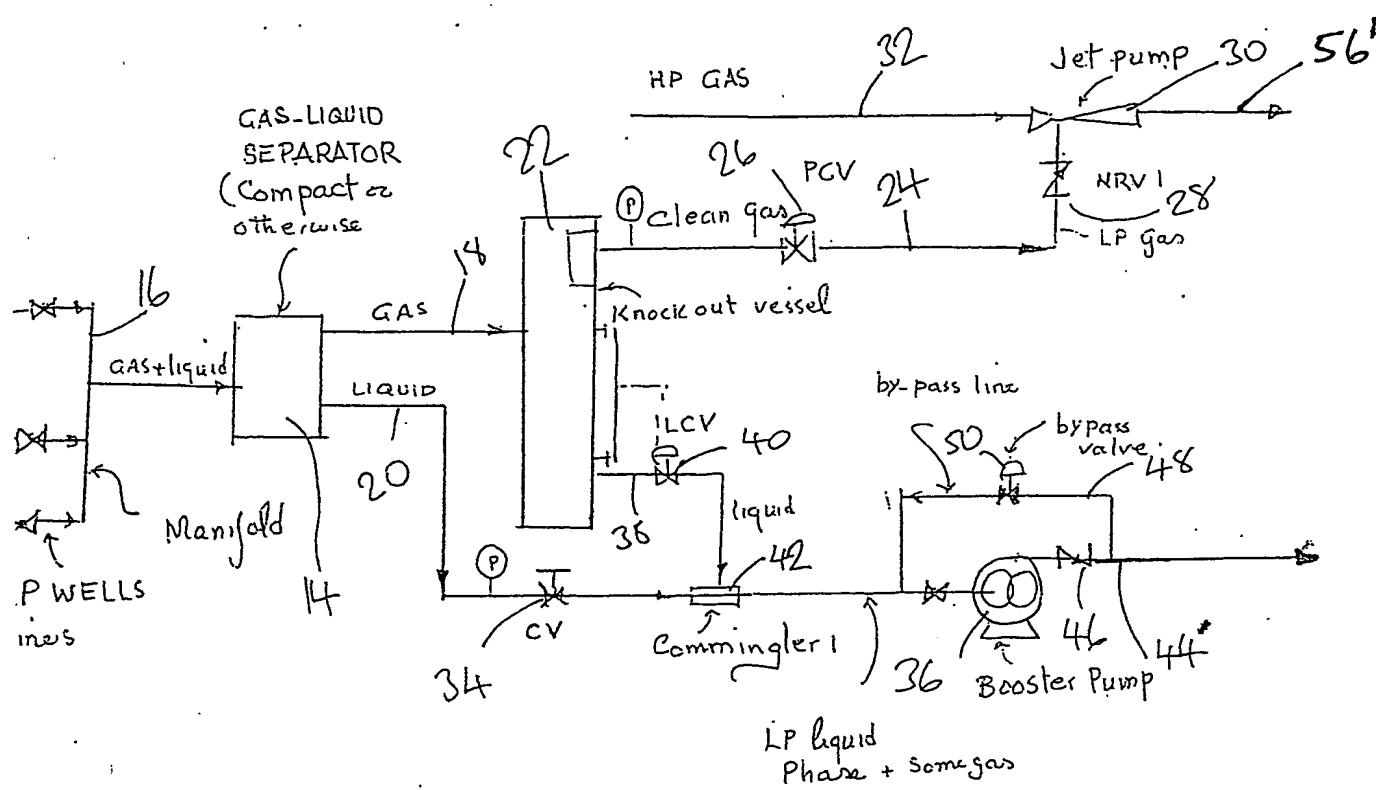


FIGURE 4

**This Page is Inserted by IFW Indexing and Scanning
Operations and is not part of the Official Record**

BEST AVAILABLE IMAGES

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images include but are not limited to the items checked:

- BLACK BORDERS**
- IMAGE CUT OFF AT TOP, BOTTOM OR SIDES**
- FADED TEXT OR DRAWING**
- BLURRED OR ILLEGIBLE TEXT OR DRAWING**
- SKEWED/SLANTED IMAGES**
- COLOR OR BLACK AND WHITE PHOTOGRAPHS**
- GRAY SCALE DOCUMENTS**
- LINES OR MARKS ON ORIGINAL DOCUMENT**
- REFERENCE(S) OR EXHIBIT(S) SUBMITTED ARE POOR QUALITY**
- OTHER:** _____

IMAGES ARE BEST AVAILABLE COPY.

As rescanning these documents will not correct the image problems checked, please do not report these problems to the IFW Image Problem Mailbox.